

CONCRETE PAVEMENT DESIGN WHAT HAVE WE LEARNED

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ACPA-SE CHAPTER**

**SOUTHEASTERN STATES PAVEMENT MANAGEMENT AND DESIGN CONFERENCE
North Little Rock, Arkansas June 3, 2008**

PAVEMENT DESIGN

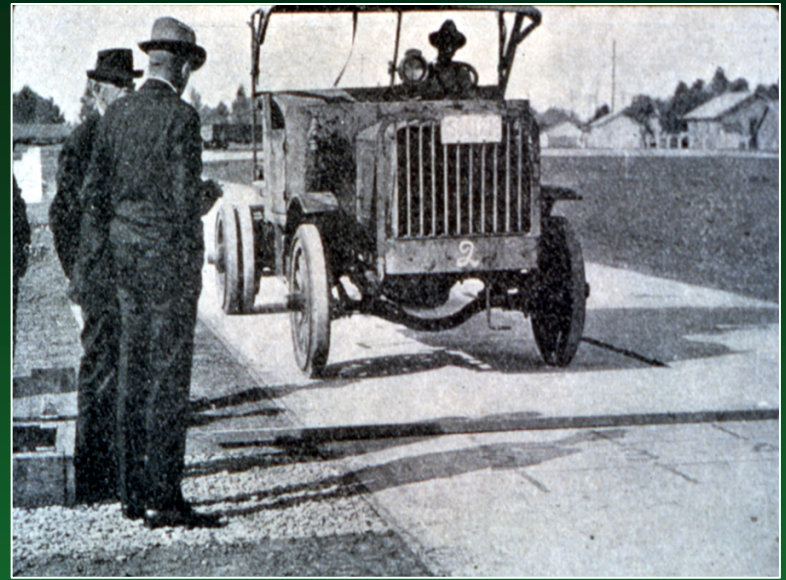
- Pavement design is an “a priori” process.
The new pavement will be built in the future, on subgrades often not yet exposed or accessible; using materials not yet manufactured from sources not yet identified; by a contractor who submitted the successful "low dollar" bid, employing unidentified personnel and procedures under climatic conditions that are frequently less than ideal.

Historical Overview of Pavement Design

Bates Road Test

- In 1920, Illinois passed a \$200 million bond issue to build 9000 miles of paved roads
- To determine the best paving material, they built sections of brick, asphalt, and concrete
- Developed thickness design procedures and chose concrete for the Illinois pavements

Old WWI Army trucks
with 9000# wheel loads



1921-23 Pittsburgh Road Test

- Pittsburgh Steel conducted tests in Pittsburgh, CA on plain and reinforced pavements.
- Hoped to prove that reinforced concrete was better



Additional Road Tests

- Maryland Road Test
 - Set up on existing concrete pavement
 - Set up between truckers and railroad operators to see who was paying their fair share of taxes.
- WASHO Road Test
 - All new asphalt pavements



AASHO Road Test (1958-1960)

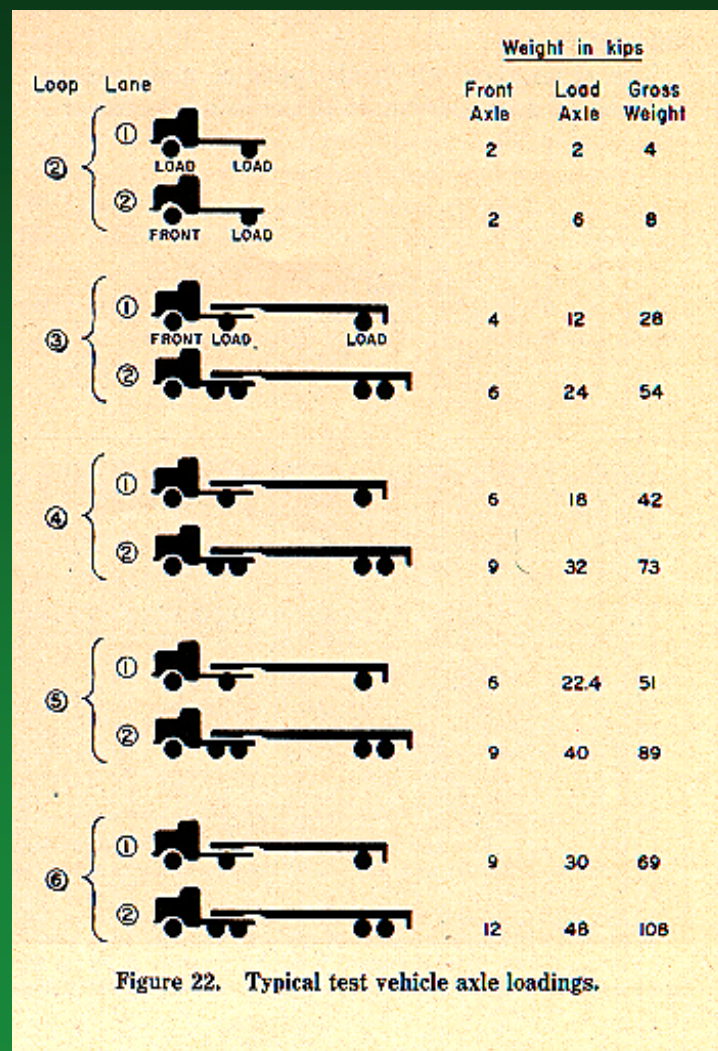
- Third Large Scale Road Test
 - Maryland Road Test (1950-51)
Rigid Pavements Only
 - WASHO Road Test (1952-54)
Flexible Pavements only
- Include both Rigid and Flexible Designs
- Include a wide range of axle loads and pavement cross-sections

Purpose of the AASHO Road Test

- Determine relationships between axle loading (type and magnitude) and pavement performance.
 - To explain performance measurements in terms of design factors.
 - To explain capability measurements in terms of design factors.
 - To determine a correlation between the various measurements of performance and capability.
 - Determine equitable cost allocation tables.

AASHO Test Traffic

- Started Nov. 1958
- Ended Dec. 1960
- Loops 3-6:
 - 6 veh/lane
 - 10 veh/lane (Jan '60)
- Operation
 - 18 hr. 40 min.
 - 6 days/wk
- Total Loads
 - 1,114,000 Applications
 - Avg. ESAL - 6.2 million
 - Max ESAL - 10 million (Flex)



AASHTO DESIGN

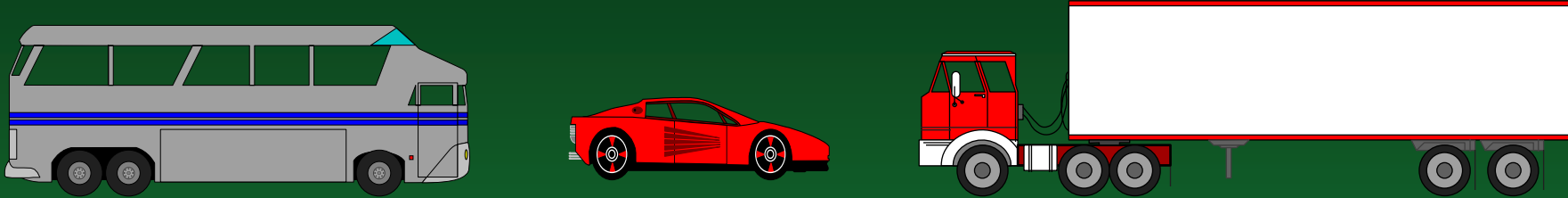
Serviceability

- **Serviceability**
 -
 - the pavement's ability to serve the type of traffic (automobiles and trucks) that use the facility

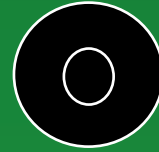
Present Serviceability Index (PSI)



REGULAR MIXED TRAFFIC



Equivalent Number of 18k Single Axle Loads



Perspective

- 1960 – Completion of Road Test Experiment
- 1961-62 Interim Guide for the Design of Rigid and Flexible Pavements
- 1972 Interim Guide for the Design of Pavements
- 1981 Revised Chapter III on Portland Cement Concrete Pavement Design
- 1986 Guide for the Design of Pavement Structures
- 1993 Revised Overlay Design Procedures
- 1998 Supplement to Concrete Design Procedures

1972 AASHTO Design Inputs

- Loadings in ESAL,s
- Initial and Terminal Serviceability
(Preset in GA)
- Concrete Flexural Strength
(working stress of 450 psi in GA)
- Concrete Modulus of Elasticity
- Support Value, k factor
- Load Transfer Coefficient
(Preset in GA)

1962 Rigid Pavement Design Equation (Georgia)

$$\text{Log(ESAL)} = 7.35 * \text{Log}(D + 1) - 0.06 - \frac{0.1761}{1 + \frac{1.624 * 10^7}{(D + 1)^{8.46}}}$$

$$+ (4.22 - 0.32p_t) * \text{Log} \left[\frac{f'_c}{(215.63 * J)} \left[\frac{D^{0.75} - 1.132}{D^{0.75} - \frac{18.42}{(E_c / k)^{0.25}}} \right] \right]$$

Preset at 3.42

(690)preset

1993 AASHTO Additional Design Inputs

Drainage Factor

Reliability Factor

Overall Deviation

Edge Support

1993 Rigid Pavement Design Equation

$$\begin{aligned}
 \text{Log(ESALs)} = & Z_R * s_o + 7.35 * \text{Log}(D + 1) - 0.06 + \left[\frac{\text{Log} \left[\frac{\Delta \text{PSI}}{4.5 - 1.5} \right]}{1 + \frac{1.624 * 10^7}{(D + 1)^{8.46}}} \right] \\
 & + (4.22 - 0.32p_t) * \text{Log} \left[\frac{S'_c * C_d * [D^{0.75} - 1.132]}{215.63 * J * \left[D^{0.75} - \frac{18.42}{(E_c / k)^{0.25}} \right]} \right]
 \end{aligned}$$

Standard Normal Deviate $\rightarrow Z_R$
 Overall Standard Deviation $\rightarrow s_o$
 Depth $\rightarrow D$
 Change in Serviceability $\rightarrow \Delta \text{PSI}$
 Terminal Serviceability $\rightarrow p_t$
 Modulus of Rupture $\rightarrow S'_c$
 Drainage Coefficient $\rightarrow C_d$
 Load Transfer $\rightarrow J$
 Modulus of Elasticity $\rightarrow E_c$
 Modulus of Subgrade Reaction $\rightarrow k$

DESIGN FEATURES OF CONCRETE PAVEMENTS (Until mid 70's)

- **9 INCH or 10 INCH THICKNESS**
- **ERODIBLE BASES**
- **UNDOWELLED JOINTS**
- **LONG SLAB LENGTHS (30ft)**
- **HOT POUR JOINT SEALS**
- **ASPHALT SHOULDERS**

I-475

- OPENED TO TRAFFIC 1966/1967
- 9 INCH THICK PCC
- NO DOWELS, 30 FT JOINT SPACING
- SOIL/ BIT STAB. BASE
- DESIGNED FOR 3.25 MILLION ESAL'S
- CARRIED ±15 MILLION at 1st CPR IN 1980. (± 50 MILLION TOTAL)

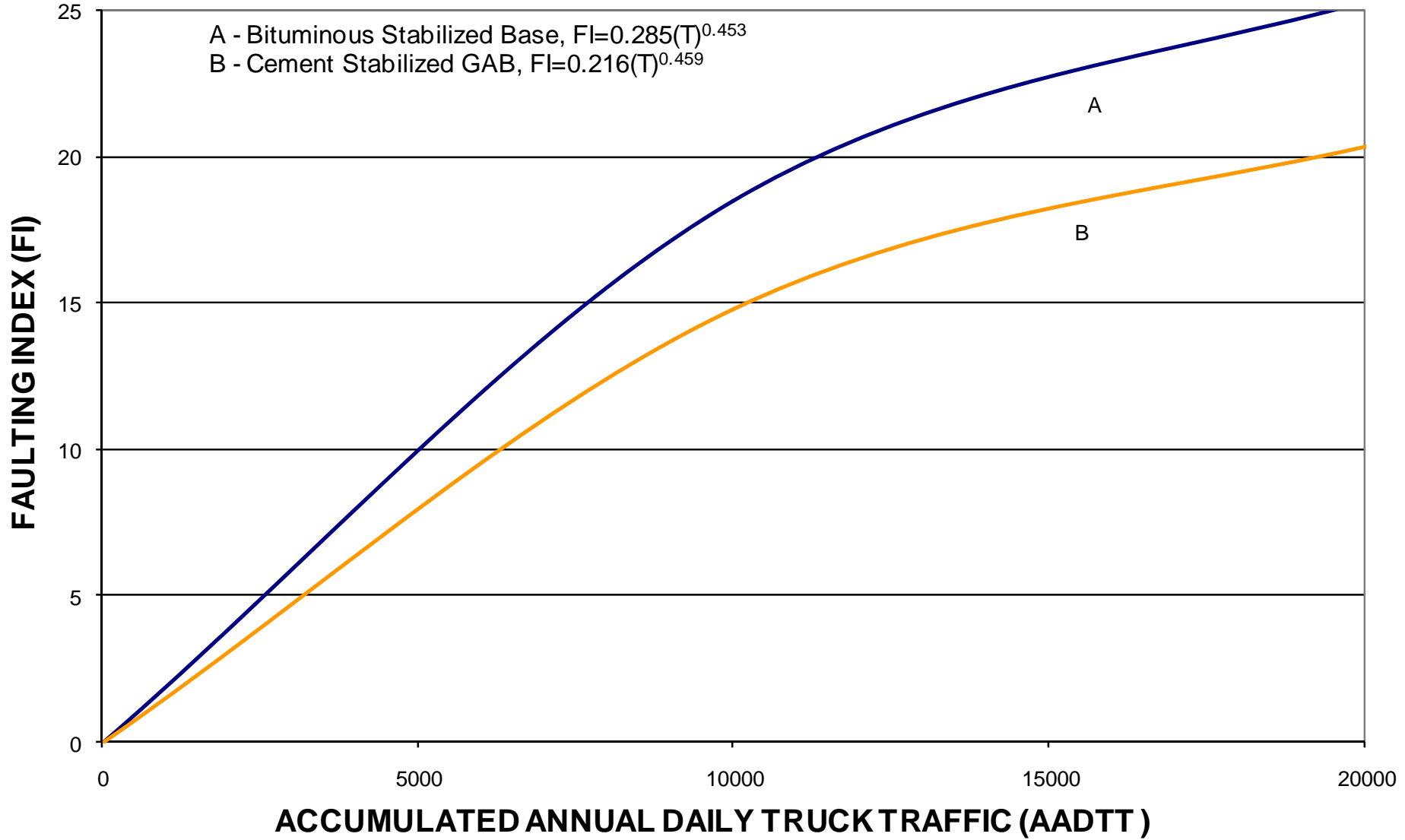
I-285

From I-20 to Chamblee-Tucker Road

- Opened to Traffic 1967/1968
- 10 inches Thickness
- No dowels. 30 ft joint spacing
- Inside lane added 1981
- Design Loads 6 million ESAL's
- CPR in 1981 at 23 million ESAL,s
- Current est. ESAL's 140 million

PCC PAVEMENT FAULTING PERFORMANCE

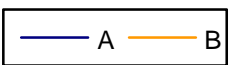
Georgia



A - Bituminous Stabilized Base, $FI=0.285(T)^{0.453}$
B - Cement Stabilized GAB, $FI=0.216(T)^{0.459}$

A

B

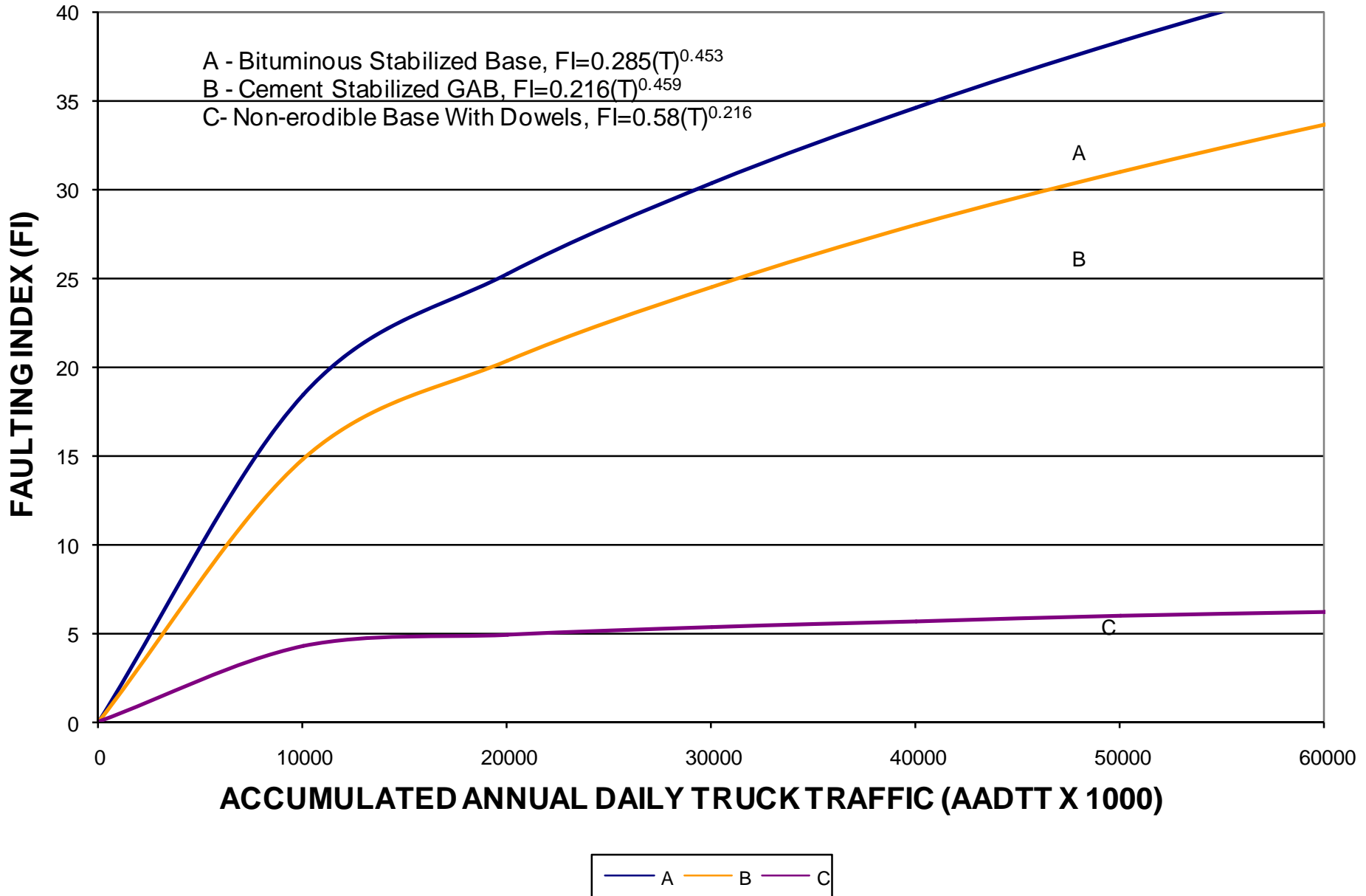


CONCRETE PAVEMENT DESIGNS (SINCE MID 70'S)

- **NON-ERODIBLE BASE**
- **DOWELLED JOINTS**
- **SHORTER JOINT SPACING**
- **TIED CONCRETE SHOULDERS
or WIDENED LANE**
- **EFFECTIVE JOINT SEALS**

PCC PAVEMENT FAULTING PERFORMANCE

Georgia



1955



2004



South from 14th Street in 1953



South from 14th Street in 2004





ESCO INC.
Truck Leasing & Rental
Chattanooga, TN

M
UNIVERSITY
800-774-4545
423-455-1100

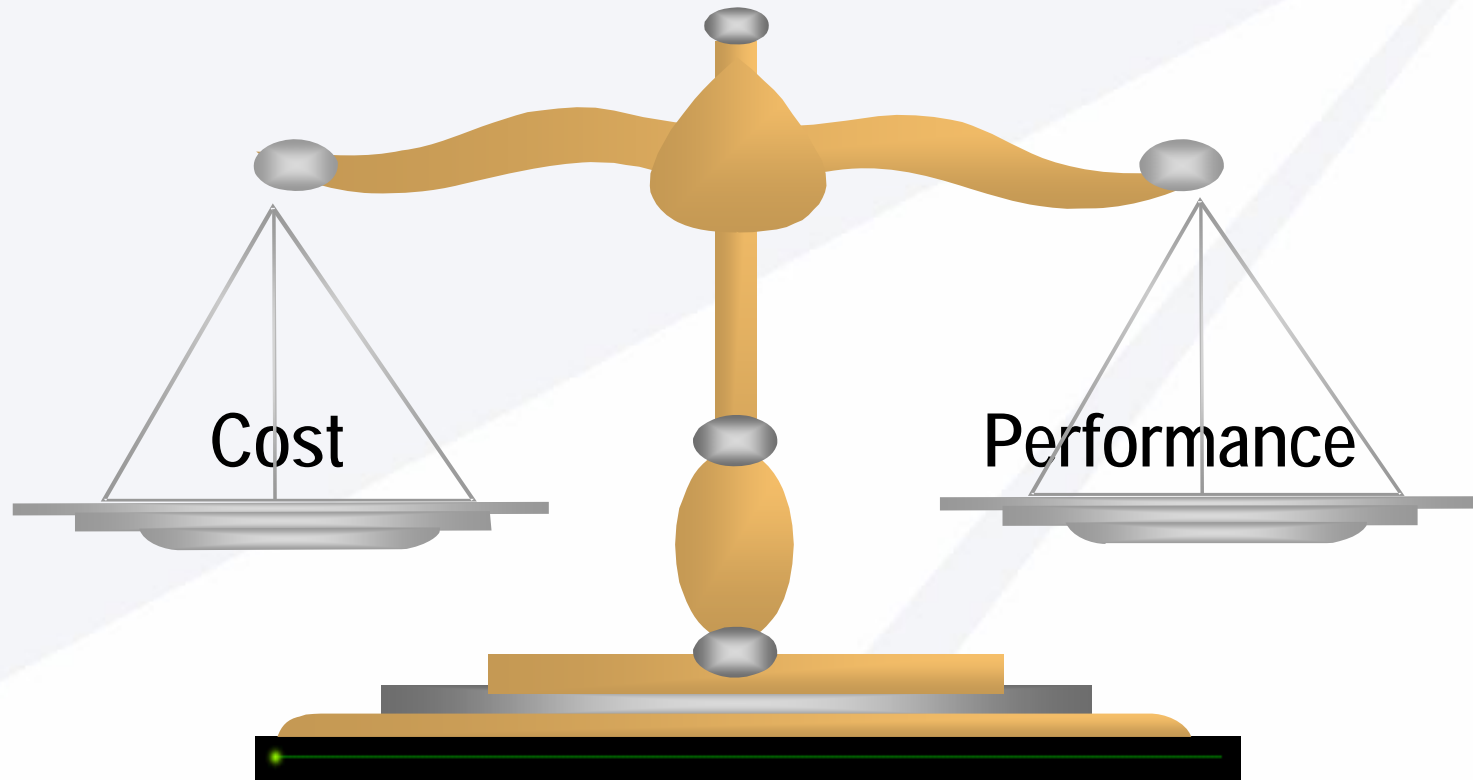
04

10R

46C-811

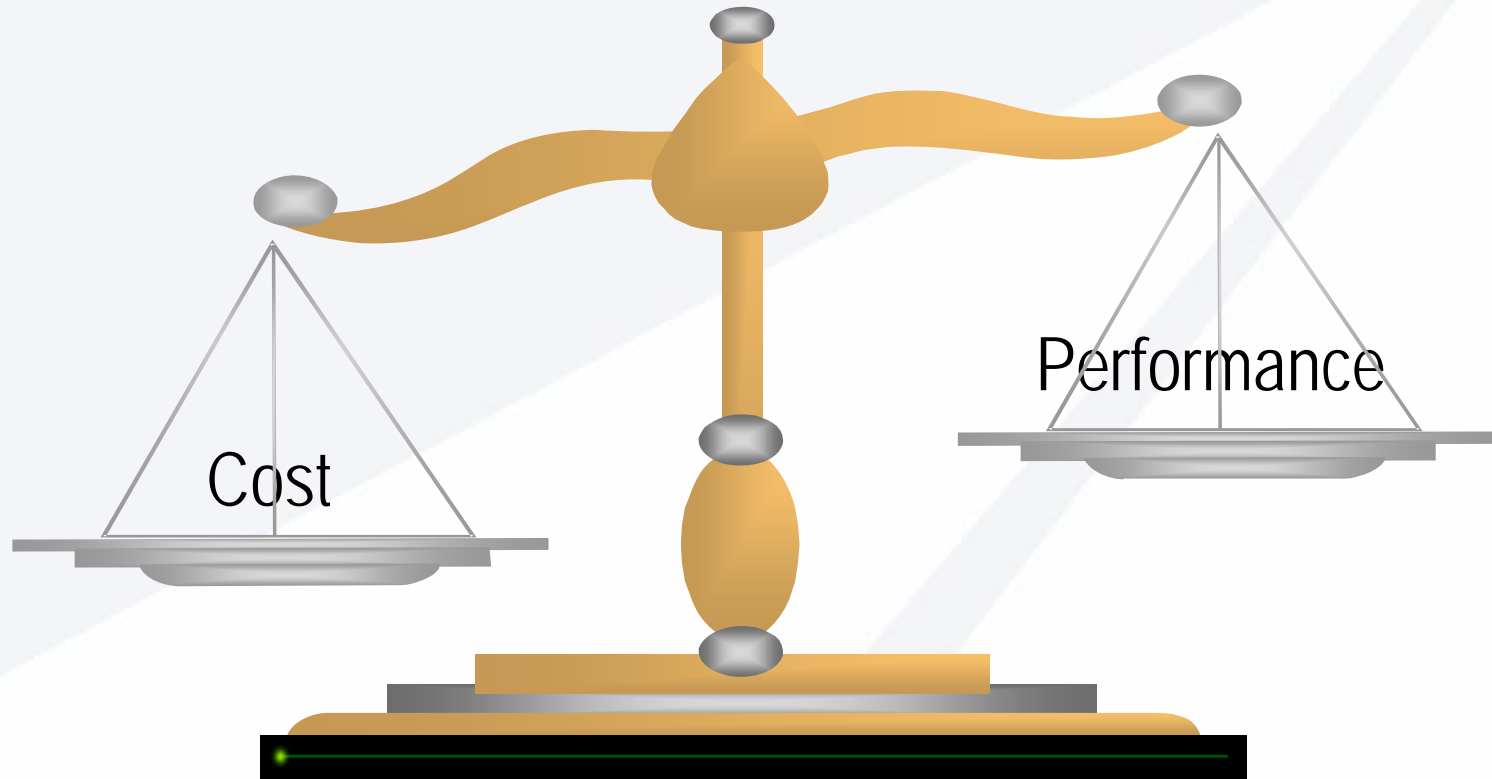


Is it about "Cheap"?





The question becomes...



What is the optimum design for the expected performance?

Cost - Performance Balance Considerations



Type of facility
Design expectations
Budget constraints

Need for Major Improvement in Pavement Design

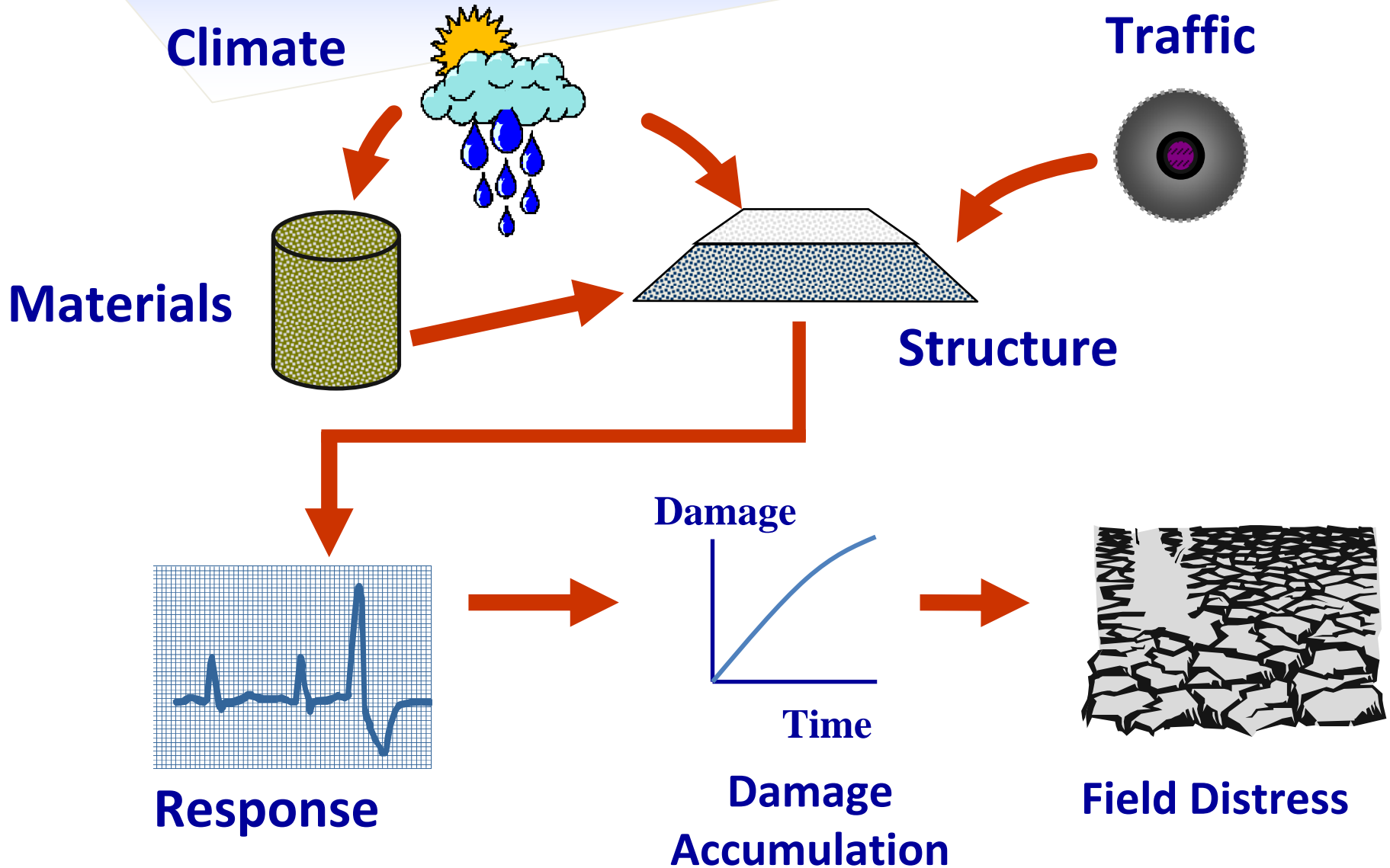
- 1990's — AASHTO Joint Task Force on Pavements realized technology and theory exist to move to mechanistic design
- 1996 NCHRP "Workshop on Improved Pavement Design" that included 70 top pavement engineers concluded this could, and should, be accomplished by 2002



Dodge

ONTARIO
WAS = HIS
L100123456

Pavement Design Factors






NCHRP

M-E PDG

Mechanistic-Empirical Pavement Design Guide


This software is for review only and should not be used for design.
This software was developed under NCHRP 1-37A and 1-40D.
Distribution of this software must be approved by NCHRP.

developed by



APPLIED RESEARCH ASSOCIATES, INC

TRANSPORTATION



WWW.TRB.ORG/MEPDG

CAUTION

**THIS SIGN HAS
SHARP EDGES**

DO NOT TOUCH THE EDGES OF THIS SIGN

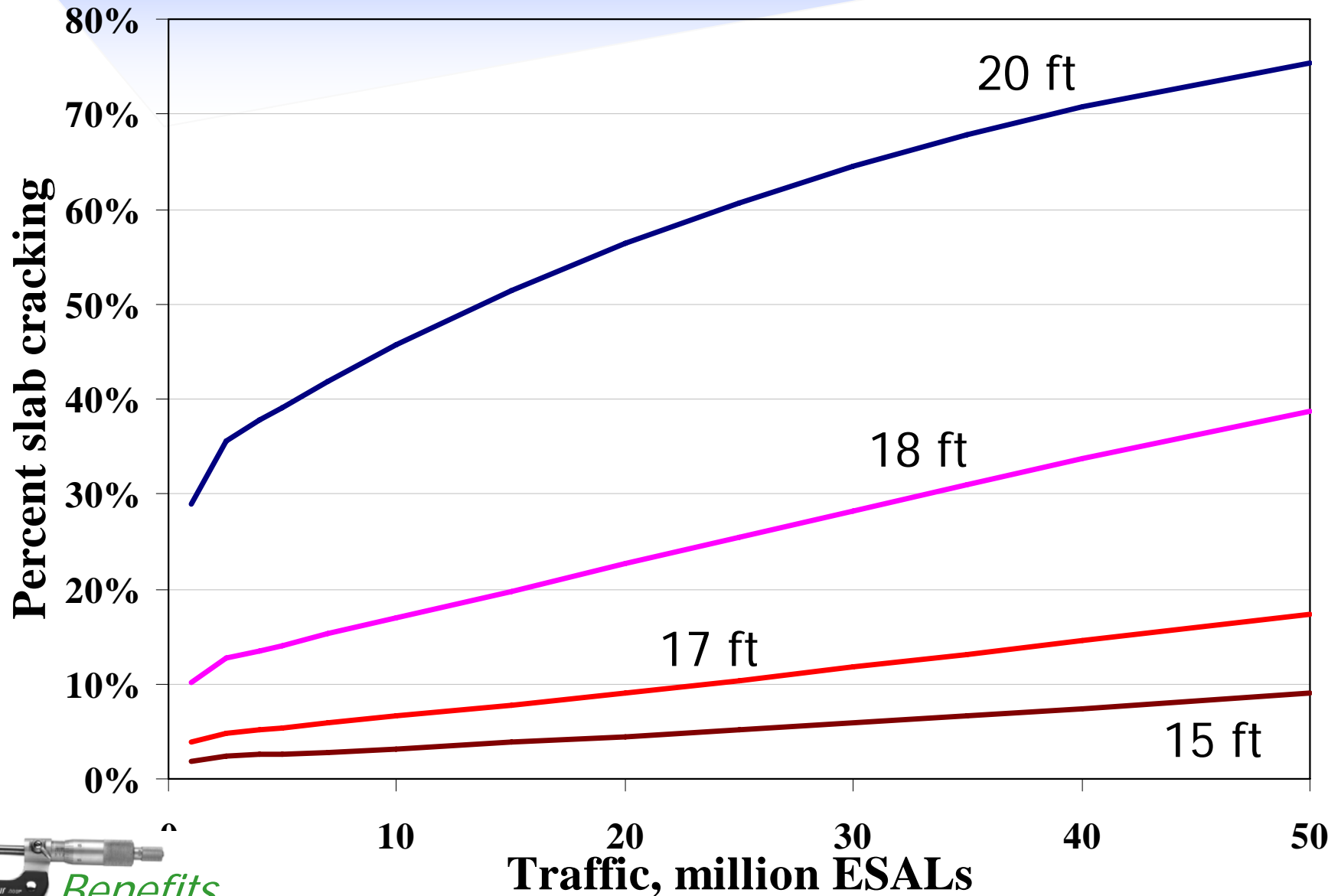


ALSO, THE BRIDGE IS OUT AHEAD

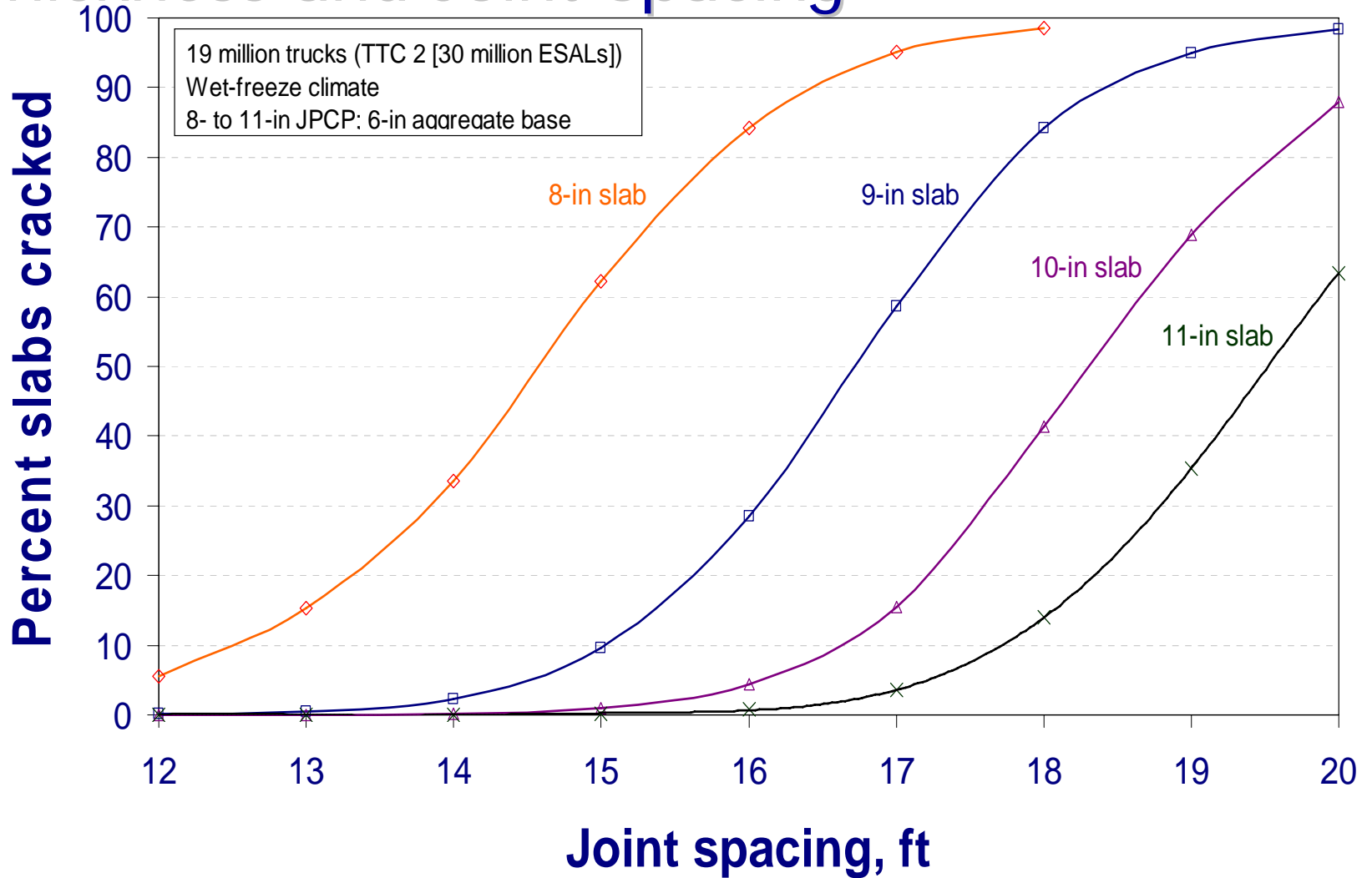




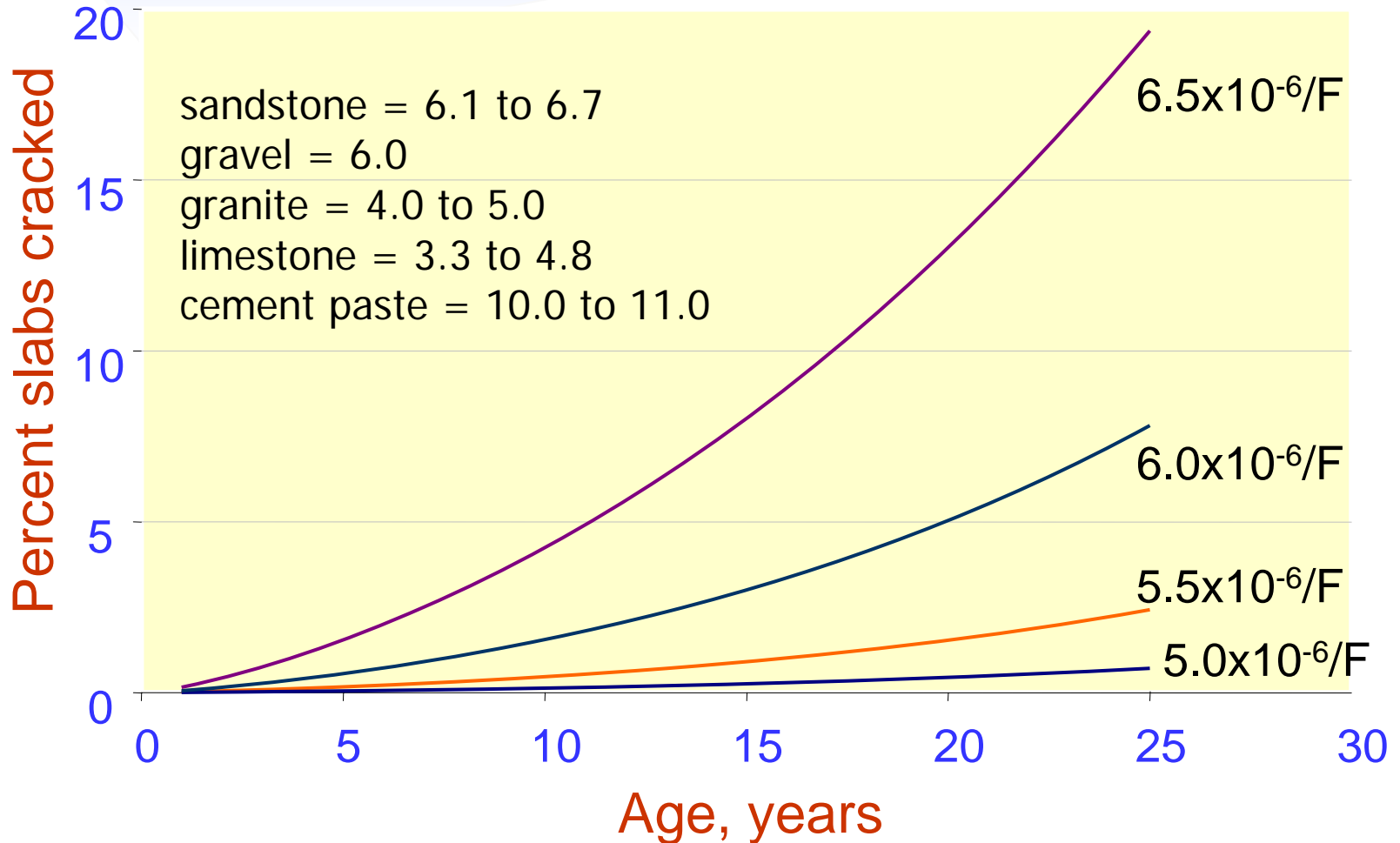
Effect of Joint Spacing



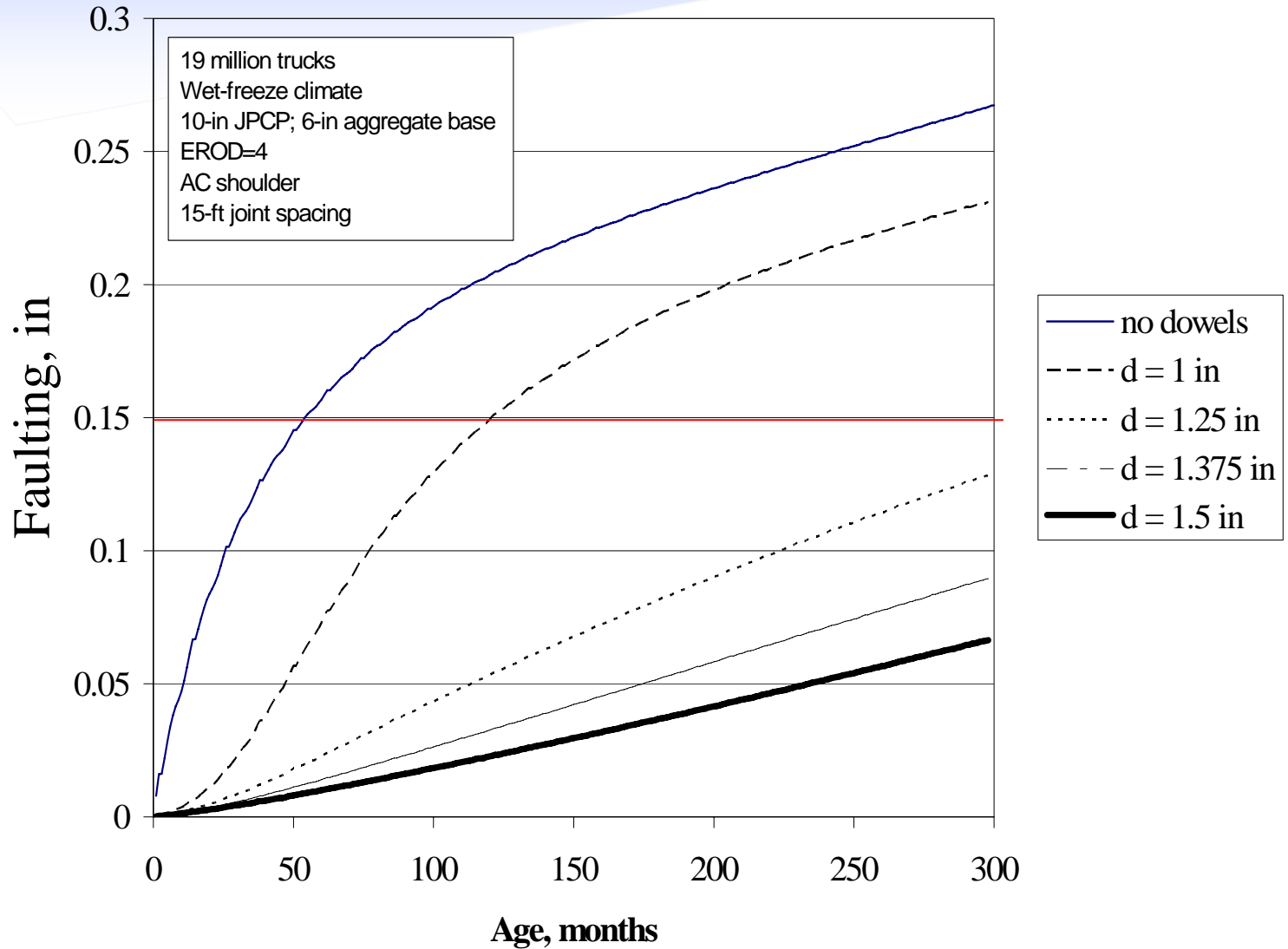
Sensitivity of JPCP Cracking to Slab Thickness and Joint Spacing



Concrete Coefficient of Thermal Expansion

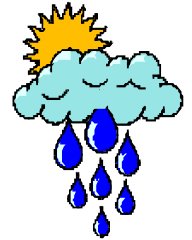


Effect of Dowel Diameter on Faulting

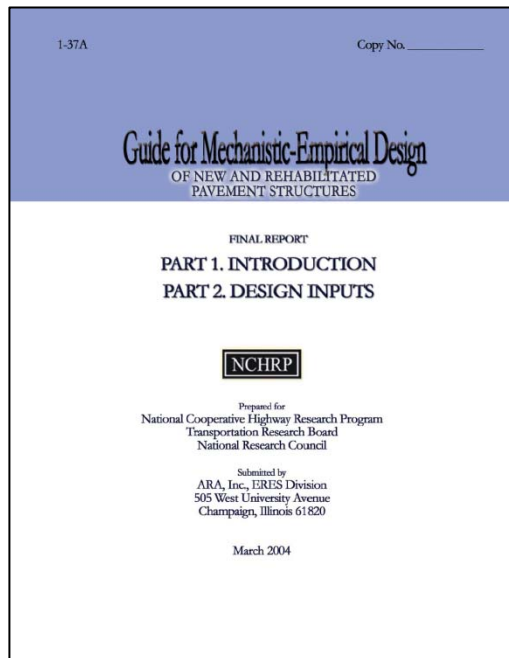


Climate and PCC Design

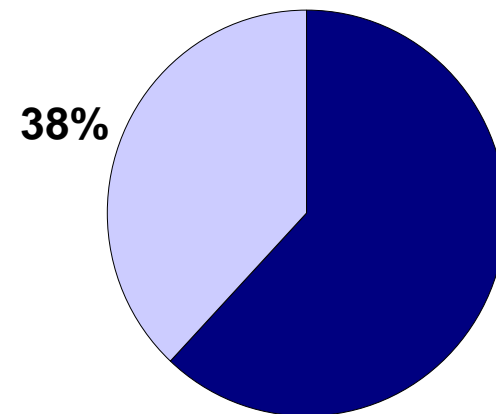
- MEPDG



Climate Inputs

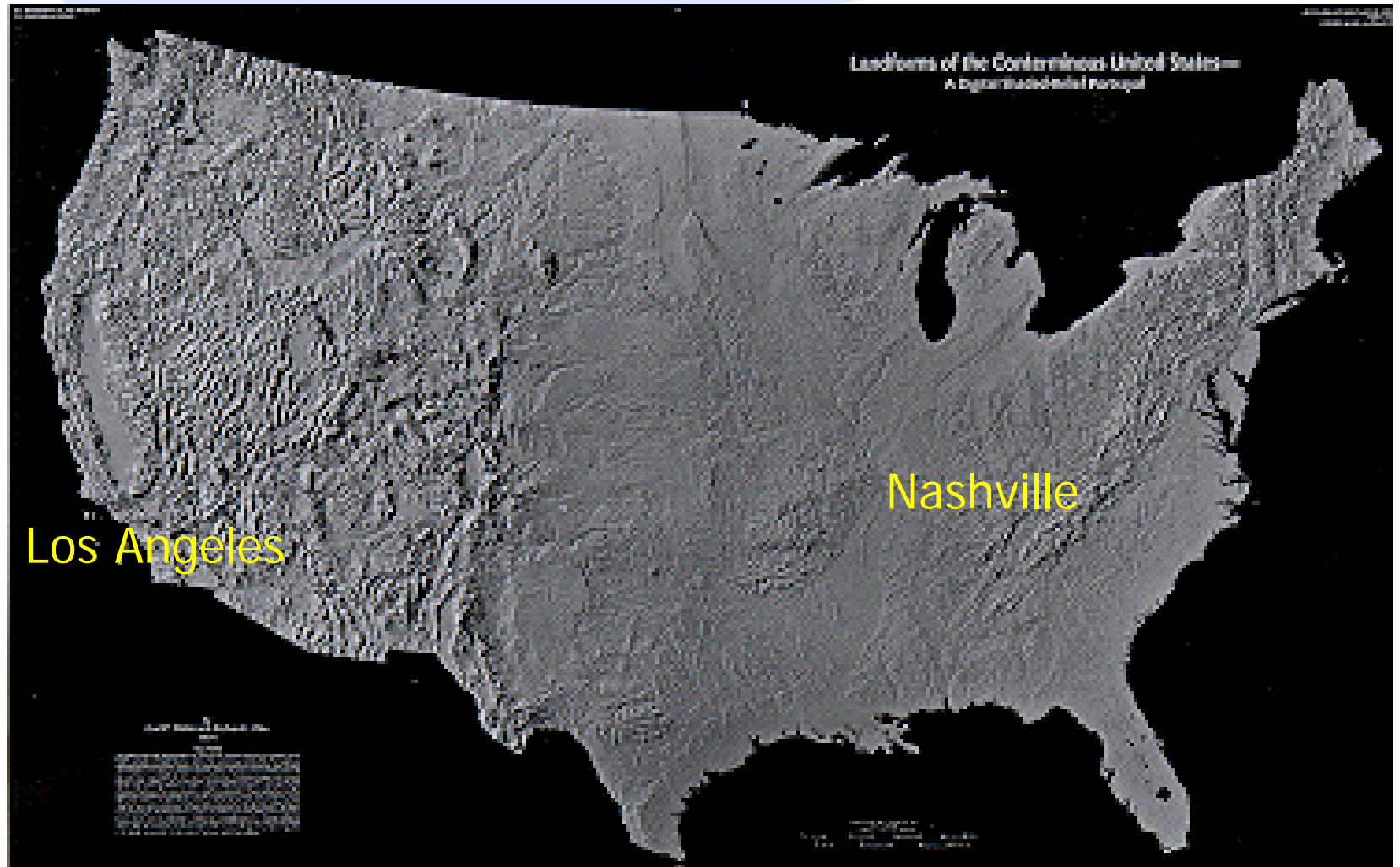


1735 Total Pages*

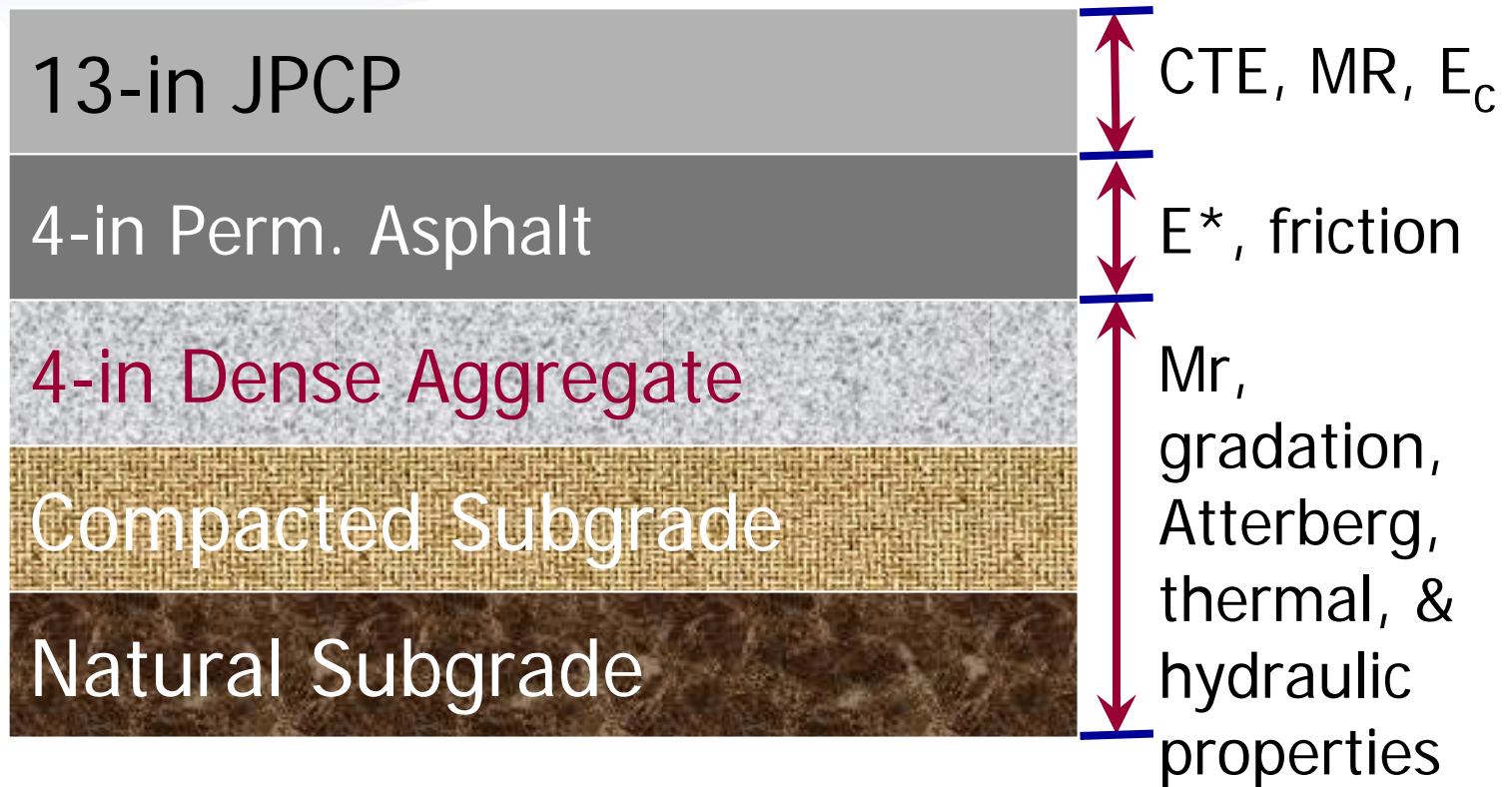


659 pages
Dedicated to Drainage
And Climate Effects

Dry Non-Freeze & Wet Freeze Climates



Project I-65 Nashville, TN



Effect of Climates

Climate Parameter	Nashville, TN	Los Angeles, CA
Mean Annual Rainfall (in)	49.96 in	14.65 in
Mean Annual Freezing Index	141 °F-days Below 32 F	0 °F-days below 32 F

Pavement Life for Thickness

Slab Thickness (in)	Location	Age when Joint Faulting > Terminal	Age when Slab Cracking > Terminal	Age when IRI > Terminal
10	Nashville	26 years	22 years	30 years
	Los Angeles	> 60 years	28 years	60 years
13	Nashville	42 years	> 60 years	46 years
	Los Angeles	> 60 years	> 60 years	> 60 years

EXAMPLE PCC PROJECT DESIGN

1981 AASHTO GUIDE (MOD 72 GUIDE)

- 4 lane divided highway
- 20 yr design loadings: 25 million ESAL,s
- $P_i = 4.5$ $P_t = 2.5$
- Base: 12 inch GAB + 3 inch AC
- K value: 290 psi
- Design Concrete Strength: 600 psi flex
– (use 450 psi in design equation)
- **Design PCC Thickness: 11.7 (use 12 inches)**

EXAMPLE PCC PROJECT DESIGN

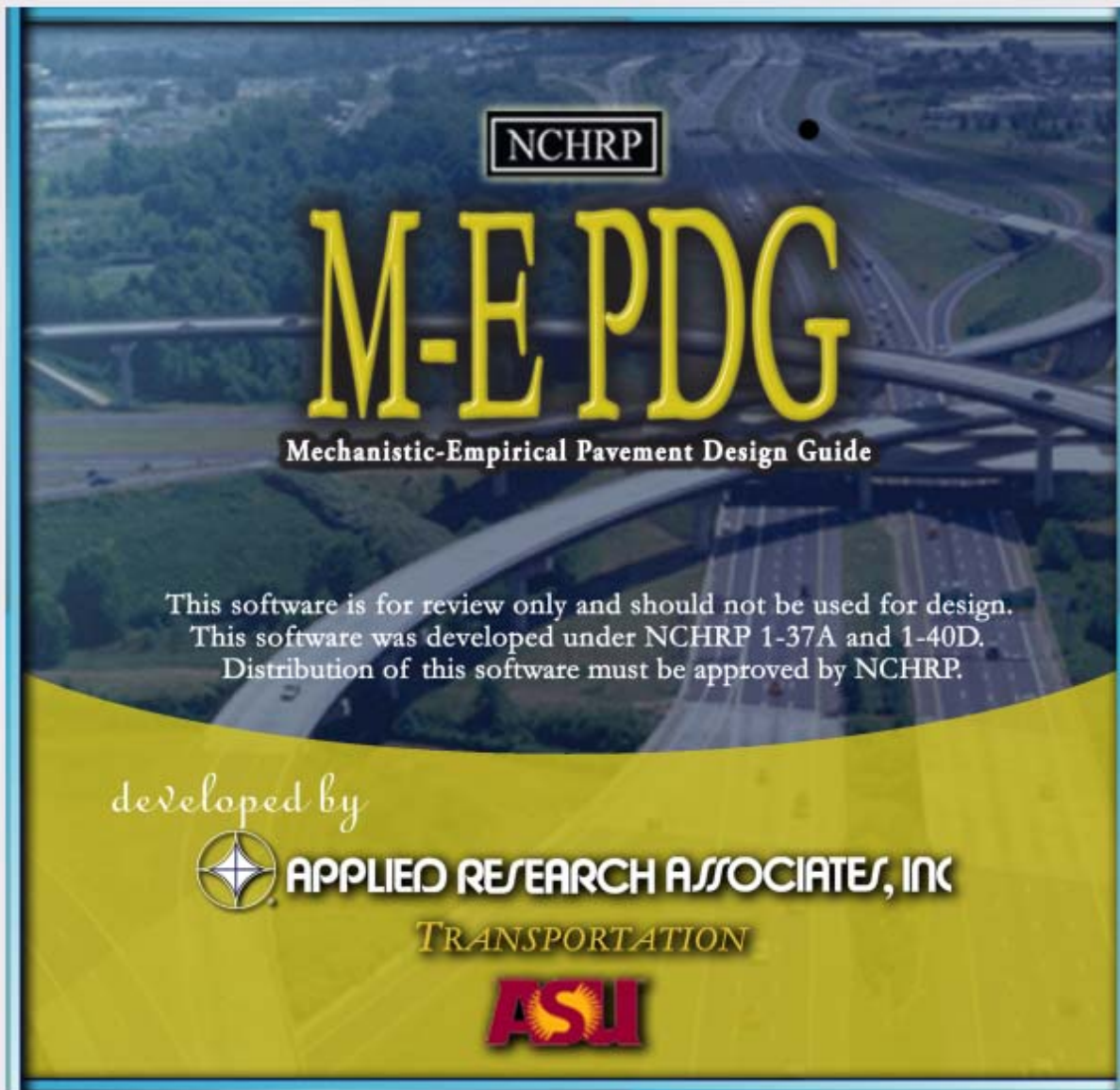
1993 AASHTO GUIDE

- 4 lane divided highway; non-interstate
- 20 yr design loadings: 25 million ESAL,s
- $P_i = 4.5$ $P_t = 2.5$
- Base: 8 inch GAB ; K value 190 psi
- Drainage factor: 1.2
- Load Transfer factor: 3.2 (dowels, no edge support)
- Reliability: 90%
- Design Concrete Strength: 600 psi flex
- Design PCC Thickness: 10.8 inches

EXAMPLE PCC PROJECT DESIGN

1993 AASHTO GUIDE

- 4 lane divided highway; non-interstate
 - 20 yr design loadings: 25 million ESAL,s
 - $P_i = 4.5$ $P_t = 2.5$
 - Base: 8 inch GAB ; K value 190 psi
 - Drainage factor: 1.2
 - Load Transfer factor: 3.2(dowels, no edge support)
 - Reliability: 90%
 - Design Concrete Strength: 690 psi flex (field strength)
 - Design PCC Thickness: 10.1 inches
- WHY NOT USE 9 INCHES**

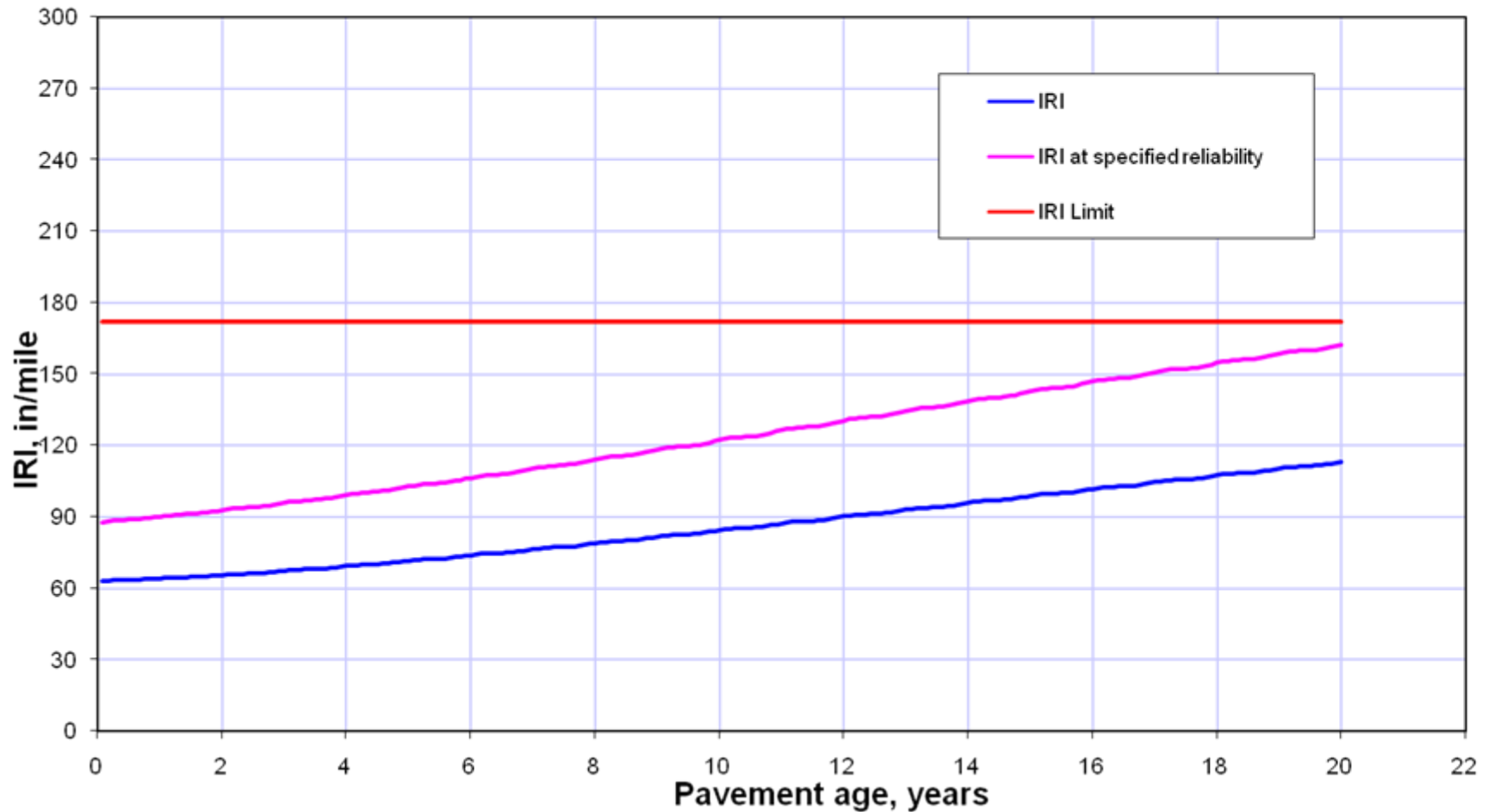


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EXAMPLE PROJECT

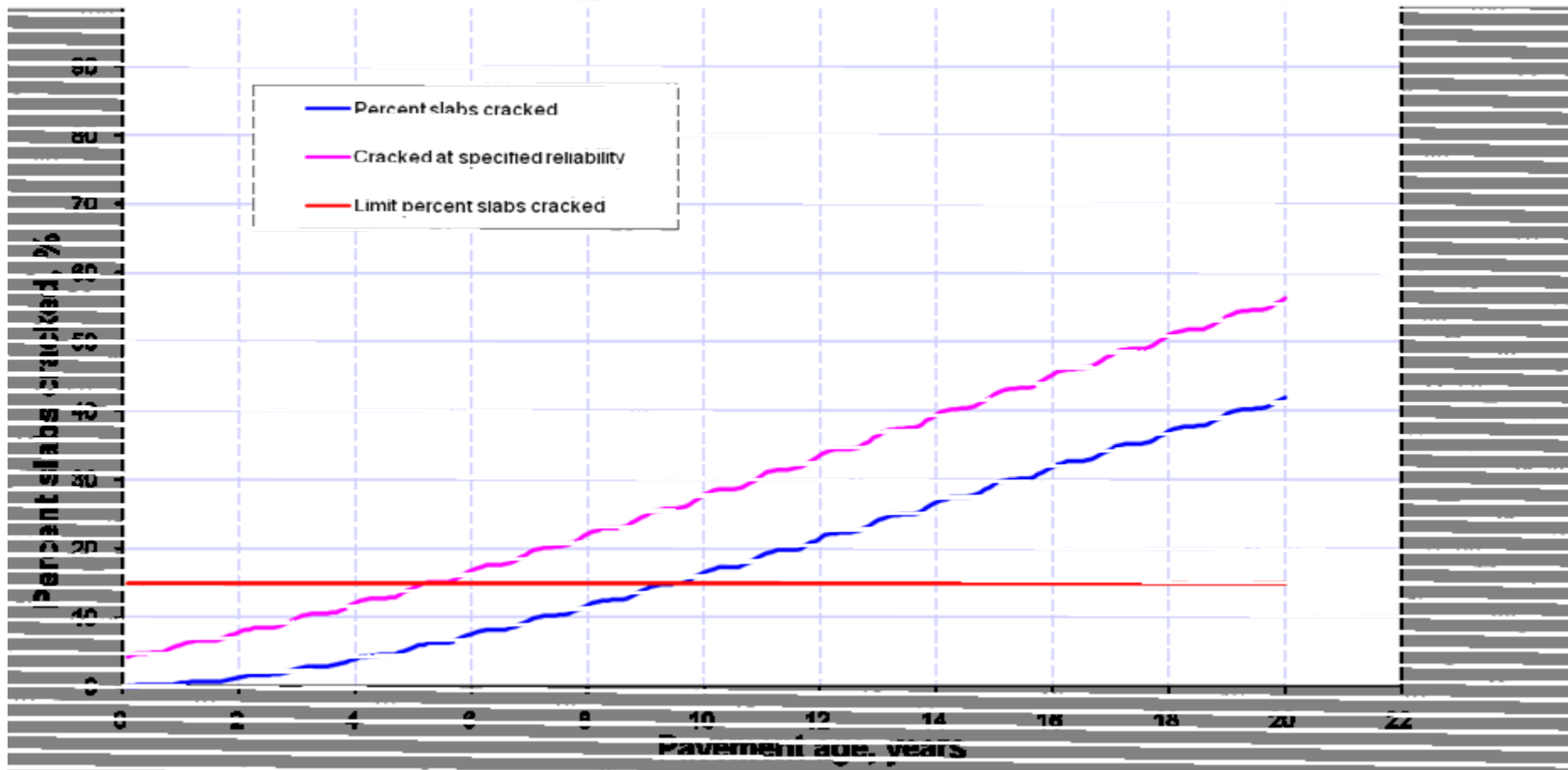
9 INCH PCC, 8 INCH GAB, 12FT OSL

Predicted IRI



EXAMPLE PROJECT

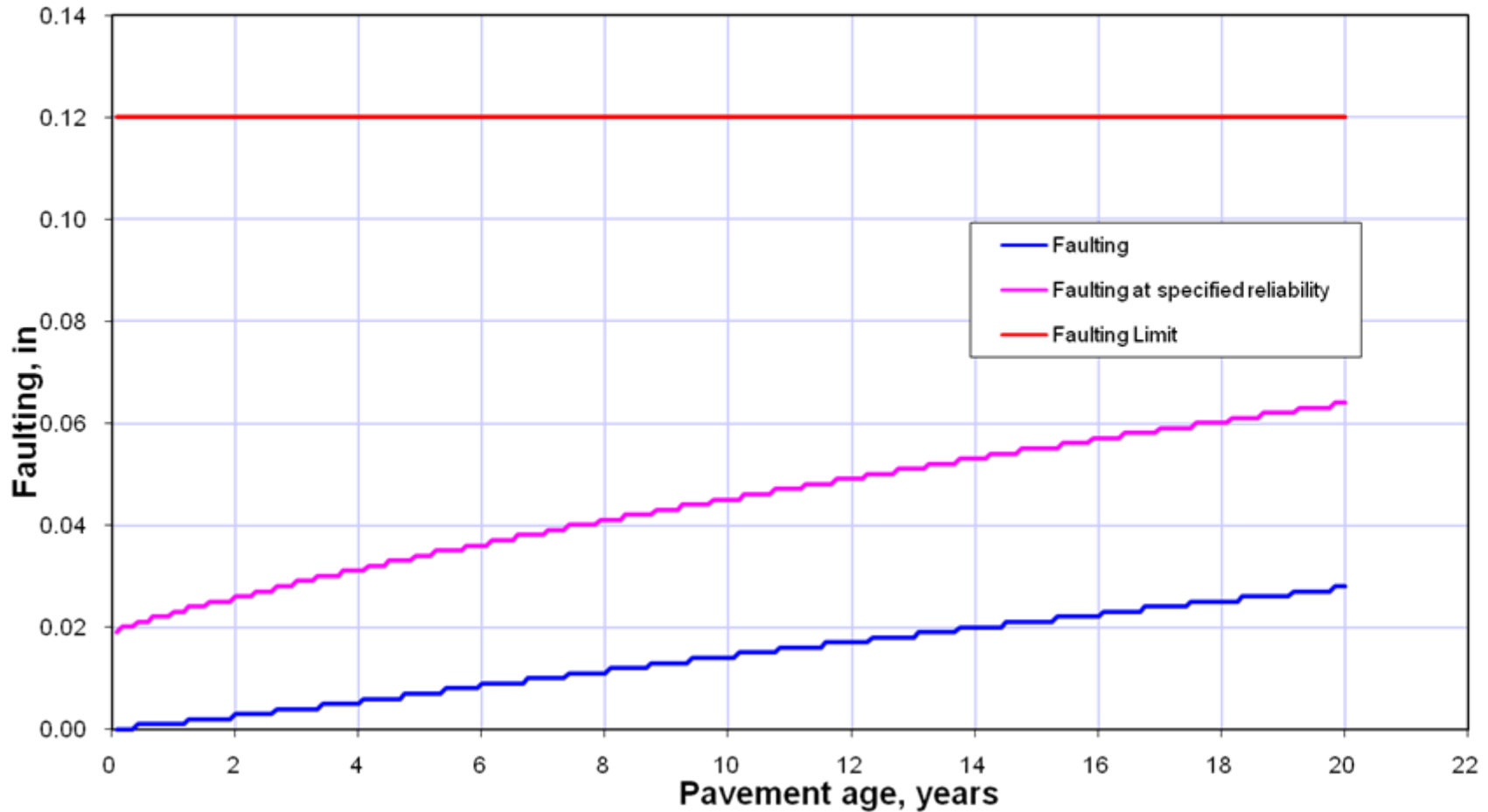
9 INCH PCC, 8 INCH GAB, 12FT OSL



EXAMPLE PROJECT

9 INCH PCC, 8 INCH GAB, 12FT OSL

Predicted Faulting



EXAMPLE PCC PROJECT DESIGN

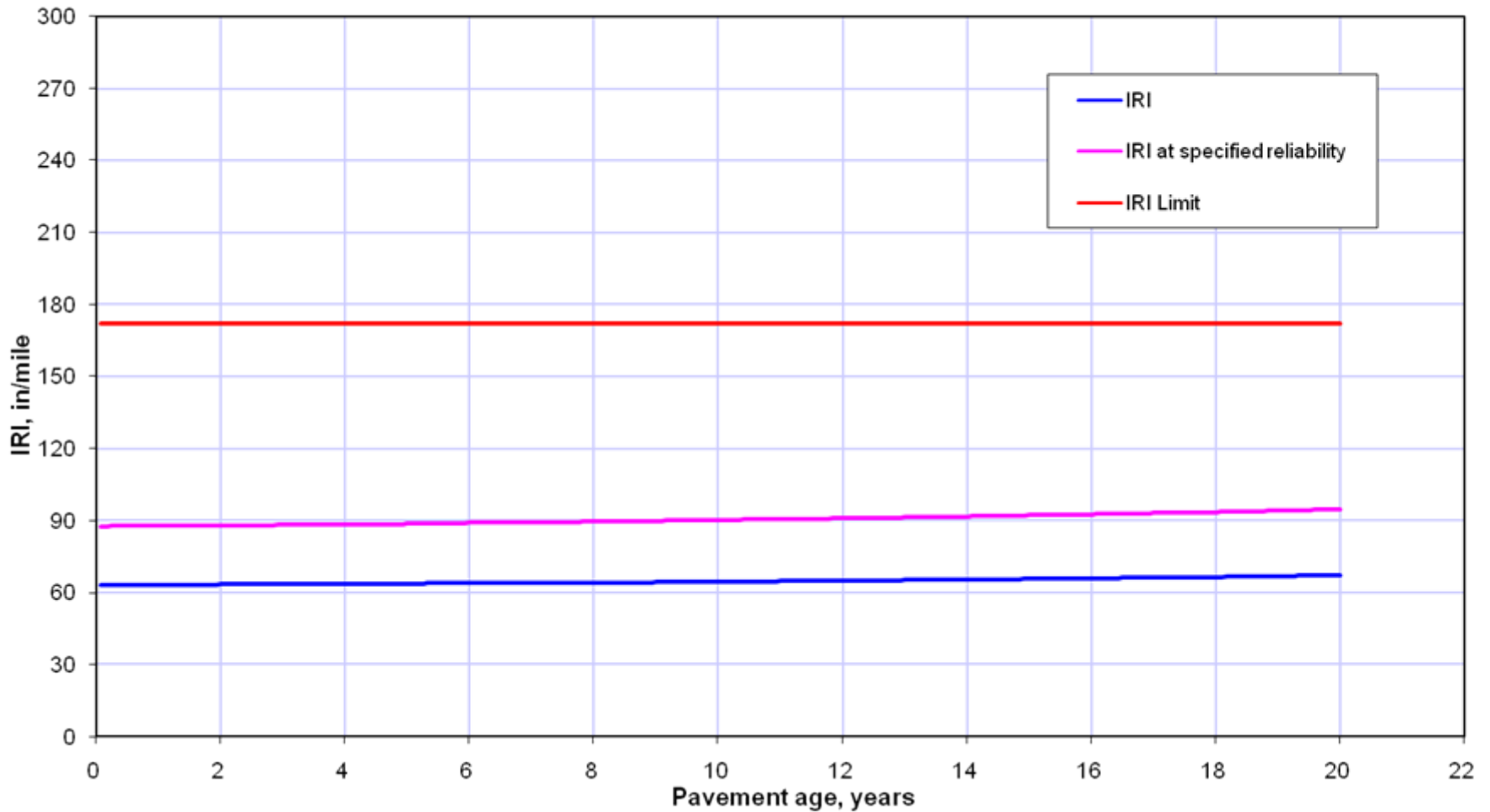
1993 AASHTO GUIDE

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- $P_i = 4.5$ $P_t = 2.5$
- Base: 8 inch GAB ; K value 190 psi
- Drainage factor: 1.2 ;
- Load Transfer factor: 2.7 (dowels, edge support)
- Reliability: 90%
- Design Concrete Strength: 690 psi flex (field strength)
- Design PCC Thickness: 9.2 inches (use 9 inches)

EXAMPLE PROJECT

9 INCH PCC, 8 INCH GAB, 13FT OSL

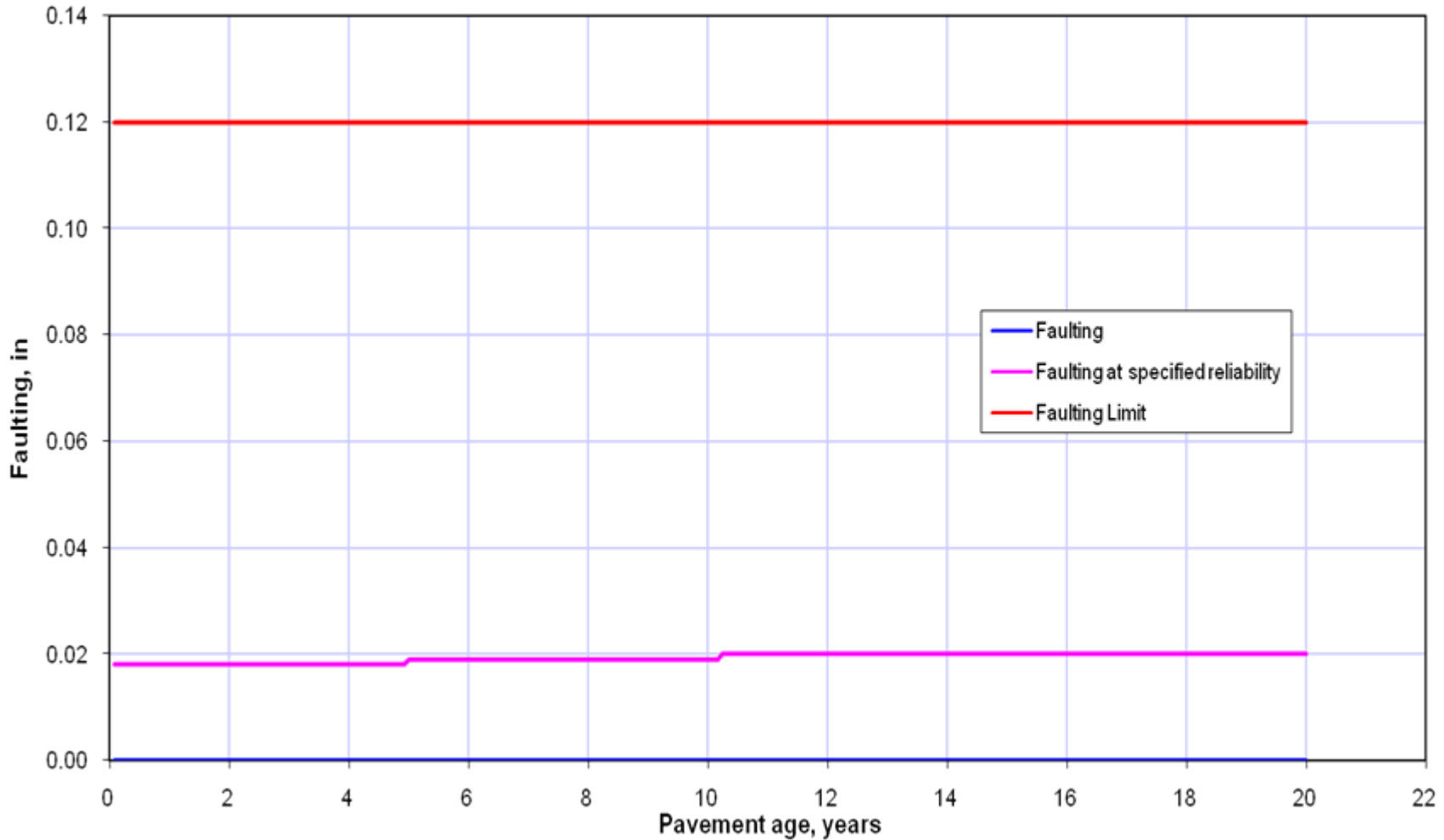
Predicted IRI



EXAMPLE PROJECT

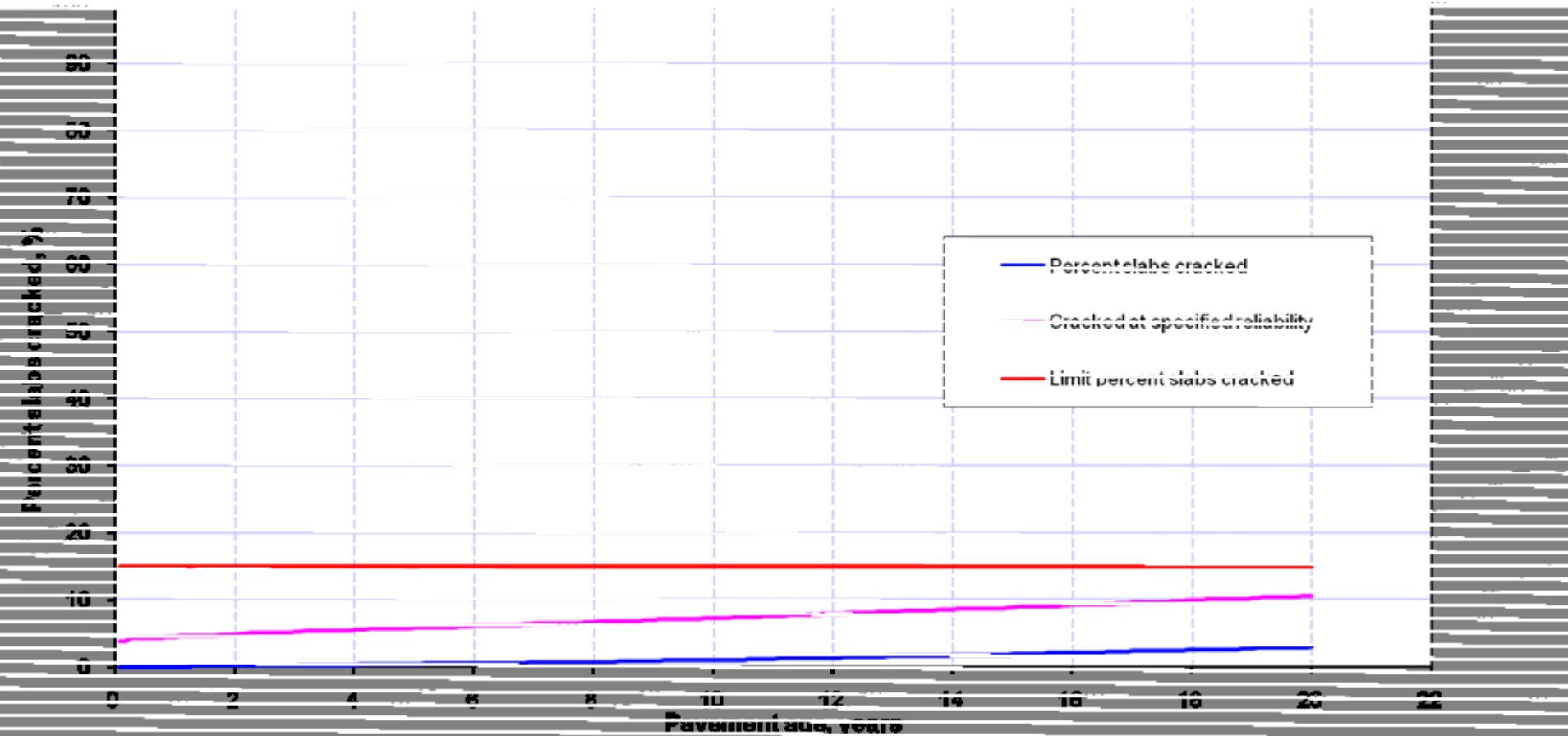
9 INCH PCC, 8 INCH GAB, 13FT OSL

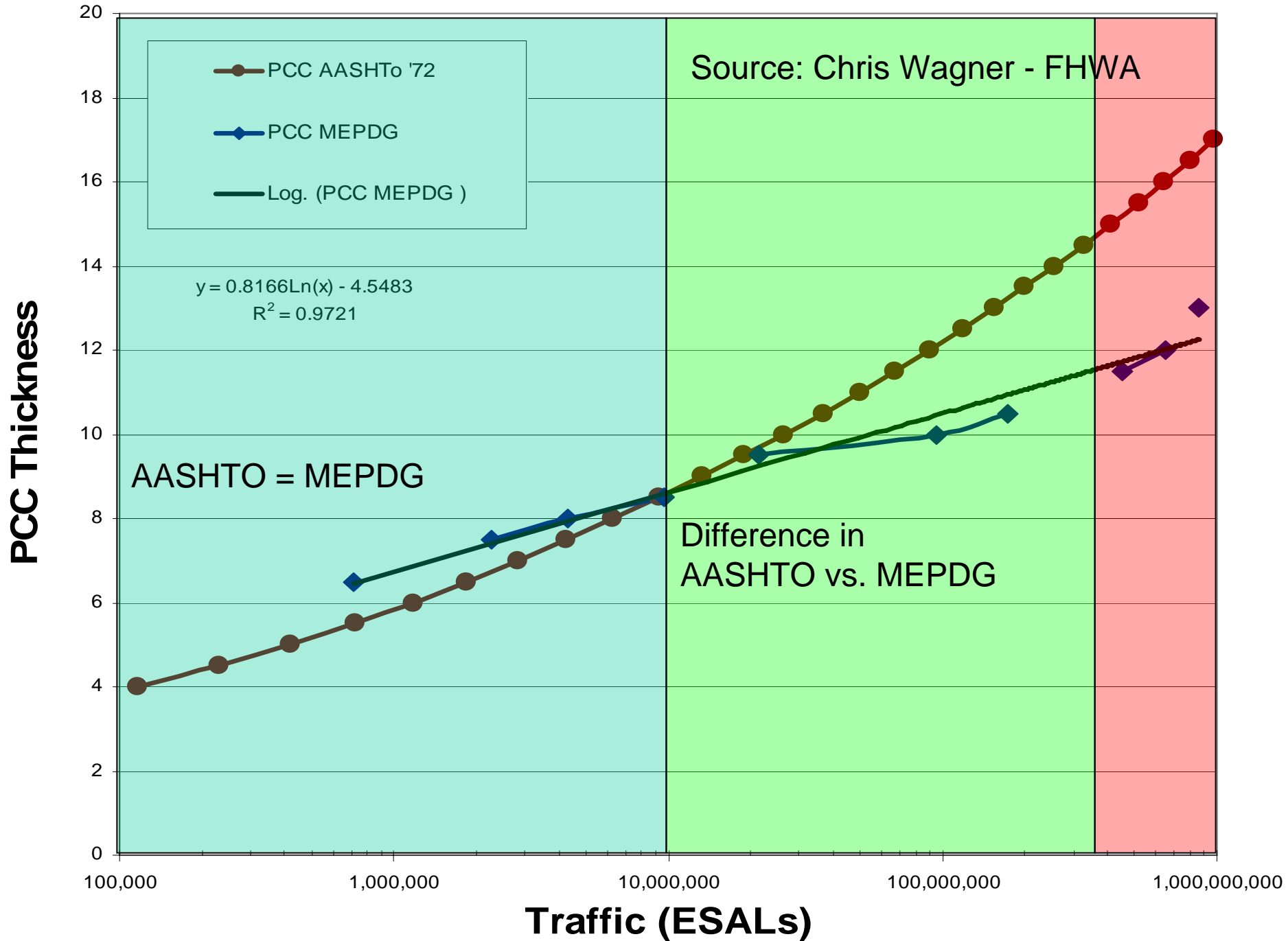
Predicted Faulting



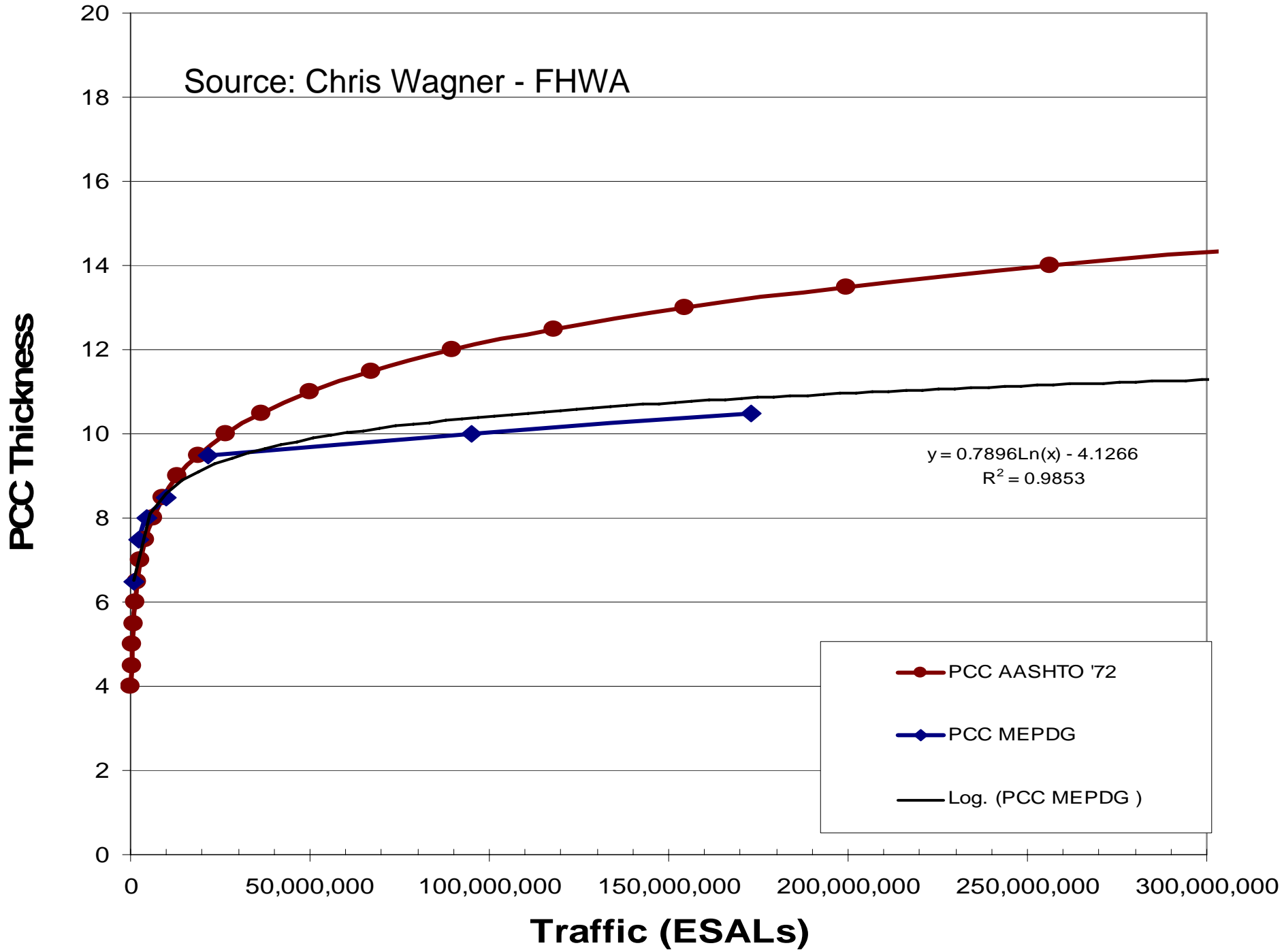
EXAMPLE PROJECT

9 INCH PCC, 8 INCH GAB, 13FT OSL





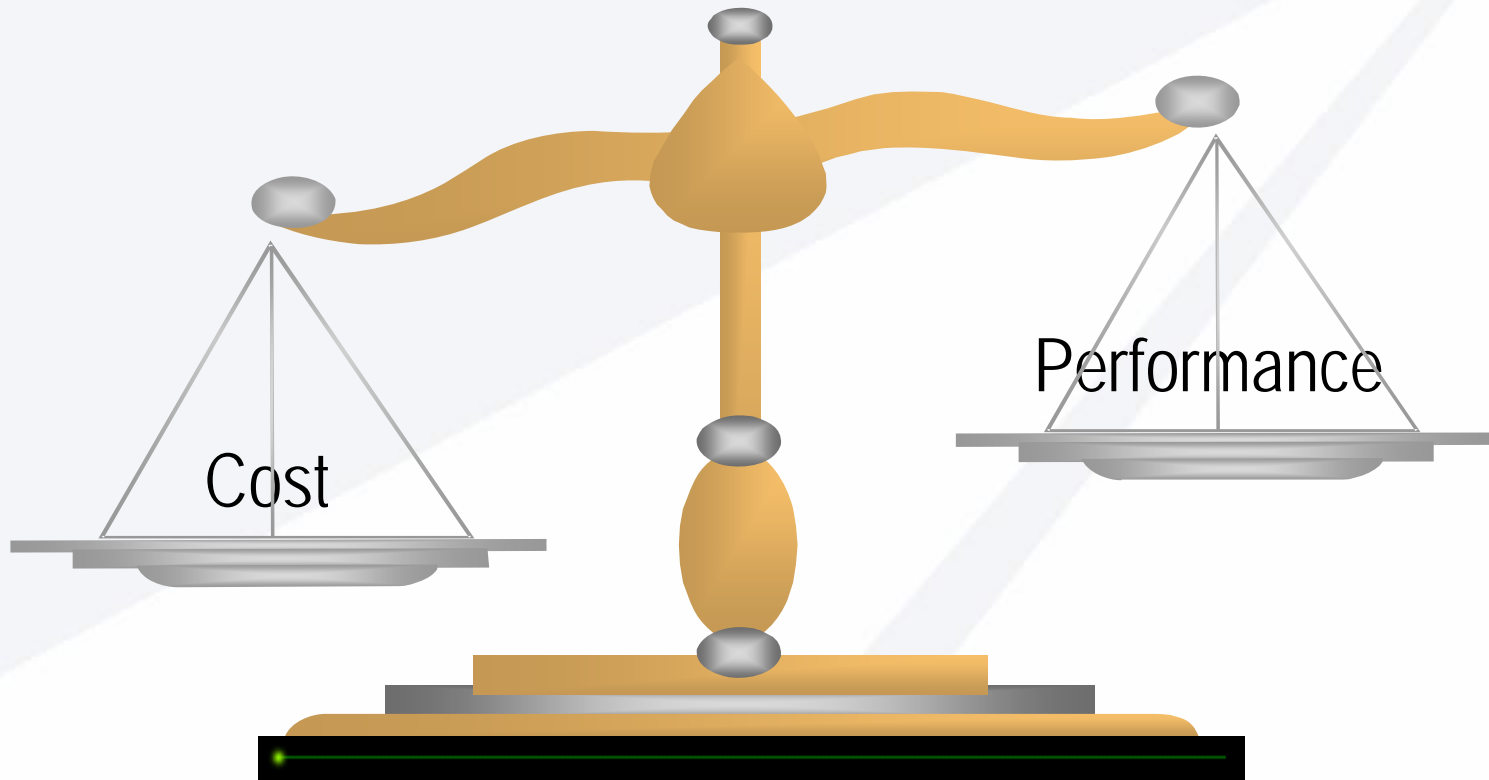
Source: Chris Wagner - FHWA



$y = 0.7896\ln(x) - 4.1266$
 $R^2 = 0.9853$

- PCC AASHTO '72
- ◆ PCC MEPDG
- Log. (PCC MEPDG)

QUESTIONS or COMMENTS



Cost-Effective Concrete Pavement Design
for the Desired Performance